## Engineered Wood Products:

LVL
PSL
LSL

- Properties

- NDS criteria
- Literature \& Design Aids
- Applications

APA - E30


## NDS - Chap. 8

8.1.2 Definitions

LVL 8.1.2.1 The term "laminated veneer lumber" refers to a composite of wood veneer sheet elements with wood fiber primarily oriented along the length of the member. Veneer thickness shall not exceed 0.25 ".
PSL 8.1.2.2 The term "parallel strand lumber" refers to a composite of wood strand elements with wood fibers primarily oriented along the length of the member. The least dimension of the strands shall not exceed $0.25^{\prime \prime}$ and the average length shall be a minimum of 150 times the least dimension.
LSL 8.1.2.3 The term "laminated strand lumber", refers to a composite of wood strand elements with wood fibers primarily oriented along the length of the member. The least dimension of the strands shall not exceed $0.10^{\prime \prime}$ and the average length shall be a minimum of 150 times the least dimension.

OSL8.1.2.4 The term "oriented strand lumber", refers to a composite of wood strand elements with wood fibers primarily oriented along the length of the member. The least dimension of the strands shall not exceed $0.10^{\prime \prime}$ and the average length shall be a minimum of 75 times the least dimension.
8.1.2.5 The term "structural composite lumber" refers to either laminated veneer lumber, parallel strand lumber, laminated strand lumber, or oriented strand lumber. These materials are structural members bonded with an exterior adhesive.


NDS - Chap. 8

Table 8.3.1 Applicability of Adjustment Factors for Structural Composite Lumber

|  |  |  | ASD and LRFD |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  | $\mathrm{K}_{\mathrm{F}}$ | $\phi$ |  |
| $F_{b}{ }^{\prime}=F_{b}$ | x | $C_{D}^{\prime}$ | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{\text {c }}$ | $\xrightarrow{\mathrm{C}_{\mathrm{L}}{ }^{1}}$ | $\mathrm{CV}^{1}$ | $\underline{C r}_{\text {r }}$ | - | - | 2.54 | 0.85 | $\lambda$ |
| $\mathrm{F}_{\mathrm{t}}^{\prime}=\mathrm{F}_{\mathrm{t}}$ | x | $\mathrm{C}_{\mathrm{D}}$ | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{1}$ | - | $\mathrm{CV}_{\mathrm{V}}$ | - | - | - | 2.70 | 0.80 | $\lambda$ |
| $\mathrm{F}_{\mathrm{v}}{ }^{\prime}=\mathrm{F}_{\mathrm{v}}$ | x | $C_{\text {d }}$ | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{1}$ | - | - | - | - | - | 2.88 | 0.75 | $\lambda$ |
| $\mathrm{F}_{\mathrm{c}}{ }^{\prime}=\mathrm{F}_{\mathrm{c}}$ | x | $\mathrm{C}_{\mathrm{D}}$ | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{1}$ | - | - | - | $\mathrm{CP}_{\mathrm{P}}$ | - | 2.40 | 0.90 | $\lambda$ |
| $\mathrm{F}_{\mathrm{c} \perp}{ }^{\prime}=\mathrm{F}_{\mathrm{c} \perp}$ | x | - | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{1}$ | - | - | - | - | $\mathrm{C}_{\mathrm{b}}$ | 1.67 | 0.90 | - |
| $E^{\prime}=E$ | x | - | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{7}$ | - | - | - | - | - | - | - | - |
| $\mathrm{E}_{\text {min }}{ }^{\prime}=\mathrm{E}_{\text {min }}$ |  | - | $\mathrm{C}_{\mathrm{M}}$ | $\mathrm{C}_{1}$ | - | - | - | - | - | 1.76 | 0.85 | - |

### 8.3.2 Load Duration Factor, $C_{D}$ (ASD Only)

All reference design values except modulus of elasticity, E, modulus of elasticity for beam and column stability, $\mathrm{E}_{\min }$, and compression perpendicular to grain, $\mathrm{F}_{\mathrm{cL}}$, shall be multiplied by load duration factors, $\mathrm{C}_{\mathrm{D}}$, as specified in 2.3.2.

### 8.3.3 Wet Service Factor, $\mathrm{C}_{\mathrm{m}}$

Reference design values for structural composite lumber are applicable to dry service conditions as specified in 8.1.4 where $\mathrm{C}_{\mathrm{M}}=1.0$. When the service conditions differ from the specified conditions, adjustments for high moisture shall be in accordance with information provided by the structural composite lumber manufacturer.

### 8.3.4 Temperature Factor, $\mathbf{C}_{t}$

When structural members will experience sustained exposure to elevated temperatures up to $150^{\circ} \mathrm{F}$ (see Appendix C), reference design values shall be multiplied by the temperature factors, $\mathrm{C}_{\mathrm{t}}$, specified in 2.3.3 .

### 8.3.5 Beam Stability Factor, $C_{L}$

Structural composite lumber bending members shall be laterally supported in accordance with 3.3.3.

### 8.3.6 Volume Factor, $\mathbf{C}_{v}$

8.3.6.1 Reference bending design values, $F_{b}$, for structural composite lumber shall be multiplied by the volume factor, $\mathrm{C}_{\mathrm{V}}$, which shall be obtained from the structural composite lumber manufacturer's literature

APA - from E30


Engineered Wood cONSTRUCTION GUIDE


Structural Composite Lumber Selection and Specification AN EXCERPI OF THE ENGINEERED WOOD CONSTRUCTION GUIDE


Slide 5 of 27

Manufactures - e.g. Weyerhaeuser


BEAMS, HEADERS, AND COLUMNS
Featuring Trus Joist ${ }^{\circledR}$ TimberStrand ${ }^{\circledR}$ LSL Microllam ${ }^{\star}$ LVL, and Parallam ${ }^{\otimes}$ PSL


Trusfoist
PARALLAM ${ }^{\oplus}$ PLUS PSL BEAMS, HEADERS
AND COLUMNS
Featuring Trus Joist ${ }^{\text {© }}$ Parallam* ${ }^{\text {© }}$ PL
with Preservative Protection


## Structural Composite Lumber



## Laminated Veneer Lumber - LVL

- Laminated Veneer Lumber (LVL)
- Veneers bonded together
- Beams, headers, rafters \& scaffold planking





## Parallel Strand Lumber - PSL

Parallel Strand Lumber (PSL):

- Manufactured from veneers clipped into long strands in a parallel formation and bonded together
- Strand length-to-thickness ratio is around 300
- Common uses: headers, beams, bearing columns
- Published on a proprietary basis by the manufacturer and in evaluation reports.



## Parallel Strand Lumber - PSL



Laminated Strand Lumber - LSL
Oriented Strand Lumber - OSL
Laminated Strand Lumber (LSL):

- Flaked strand length-to-thickness ratio is around 150
- Common uses: studs


Oriented Strand Lumber (OSL):

- Flaked strand length-to-thickness ratio is around 75
- Common uses: studs



# Field Notching and Drilling of Glulam (Form S560) Horizontal Hole Drilling 

FIGURE 3
ZONES WHERE SMALL HORIZONTAL HOLES ARE PERMITTED IN A UNIFORMLY LOADED, SIMPLY SUPPORTED BEAM

2. Zones where horizontol holes are permitred for possoge of wires, conduit, etc.

## Weyerhaeuser - Trus Joist

## LSL - LVL - PSL



This guide features Trus Joist ${ }^{\circledR}$ engineered lumber in the following widths and depths:

TimberStrand ${ }^{\circledR}$ LSL
1.55E TimberStrand ${ }^{8}$ LSL sizes:

Widths: $1^{3 / 4} 4^{\prime \prime}$ and $3^{1 / 21} 2^{\prime \prime}$
Depths: $9112^{\prime \prime}, 11^{7 / 8^{\prime \prime}}, 14^{\prime \prime}$, and $16^{\prime \prime}$
1.3E TimberStrand ${ }^{\otimes}$ LSL header sizes:

Width: $3^{1 / 2} 2^{1}$
Depths: $43 / 8^{\prime \prime}$, $51 / 2^{\prime \prime}$, and $71 / 4^{\prime \prime}$
1.3E TimberStrand ${ }^{\oplus}$ LSL column and post sizes:

Microllam ${ }^{\star}$ LVL
2.0E Microllam ${ }^{\text {® }}$ LVL header and beam sizes:

Width: $1^{3 / 4^{\prime \prime}}$

Parallam ${ }^{\circledR}$ PSL
2.0E Parallam ${ }^{\otimes}$ PSL header and beam sizes:

Widths: $3112^{2 \prime}, 5 \frac{1}{2} 4^{"}$, and 7 "
Depths: $\underline{9}^{1 / 4} 4^{\prime \prime}, 99^{1 / 2}, 11^{1 / 4 / 4}, 11^{\prime / 8^{\prime \prime}}, 14^{\prime \prime}, 16^{\prime \prime}$, and $18^{\prime \prime}$
1.8E Parallam ${ }^{\circledR}$ PSL column and post sizes:


For deeper depth Parallam ${ }^{\otimes}$ PSL beams, see the Irus Joist® 2.2E Parallam ${ }^{\otimes}$ PSL
Deep Beam guide, TJ-7001, or contact your Weyerhaeuser representative.
TJ_9000

DESIGN PROPERTIES
$C_{D}=1.0$
Allowable Design Properties ${ }^{(1)}$ (100\% Load Duration)

|  |  |  | Depth |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grade | Width | Design Property | $43 / 8^{\prime \prime}$ | 51⁄2" | $\begin{gathered} 51 / 2^{\prime \prime} \\ \text { Plank } \\ \text { Orientation } \end{gathered}$ | 71/4 ${ }^{\text {" }}$ | 91/4" | 91/2" | 111/4" | 117/8 ${ }^{\prime \prime}$ | $14^{\prime \prime}$ | $16^{\prime \prime}$ | 18" | 20" |
| TimberStrand LSL |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.3E | $31 / 2^{\prime \prime}$ | Moment (ft-lbs) | 1,735 | 2,685 | 1,780 | 4,550 |  |  |  |  |  |  |  |  |
|  |  | Shear (lbs) | 4,340 | 5,455 | 1,925 | 7,190 |  |  |  |  |  |  |  |  |
|  |  | Moment of Inertia (in. ${ }^{\text {4 }}$ ) | 24 | 49 | 20 | 111 |  |  |  |  |  |  |  |  |
|  |  | Weight (plf) | 4.5 | 5.6 | 5.6 | 7.4 |  |  |  |  |  |  |  |  |
| 1.55 E | 13/4" | Moment (ft-lbs) |  |  |  |  |  | 5,210 |  | 7,975 | 10,920 | 14,090 |  |  |
|  |  | Shear (lbs) |  |  |  |  |  | 3,435 |  | 4,295 | 5,065 | 5,785 |  |  |
|  |  | Moment of Inertia (in. ${ }^{4}$ ) |  |  |  |  |  | 125 |  | 244 | 400 | 597 |  |  |
|  |  | Weight (plf) |  |  |  |  |  | 5.2 |  | 6.5 | 7.7 | 8.8 |  |  |
|  | $31 / 2^{\text {" }}$ | Moment (ft-lbs) |  |  |  |  |  | 10,420 |  | 15,955 | 21,840 | 28,180 |  |  |
|  |  | Shear (lbs) |  |  |  |  |  | 6,870 |  | 8,590 | 10,125 | 11,575 |  |  |
|  |  | Moment of Inertia (in. ${ }^{\text {4 }}$ ) |  |  |  |  |  | 250 |  | 488 | 800 | 1,195 |  |  |
|  |  | Weight (plf) |  |  |  |  |  | 10.4 |  | 13 | 15.3 | 17.5 |  |  |
| Microllam ${ }^{\text {® LVL }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2.0 E | 13/4" | Moment (ft-lbs) |  | 2,125 |  | 3,555 | 5,600 | 5,885 | 8,070 | 8,925 | 12,130 | 15,555 | 19,375 | 23,580 |
|  |  | Shear (lbs) |  | 1,830 |  | 2,410 | 3,075 | 3,160 | 3,740 | 3,950 | 4,655 | 5,320 | 5,985 | 6,650 |
|  |  | Moment of Inertia (in. ${ }^{4}$ ) |  | 24 |  | 56 | 115 | 125 | 208 | 244 | 400 | 597 | 851 | 1,167 |
|  |  | Weight (plf) |  | 2.8 |  | 3.7 | 4.7 | 4.8 | 5.7 | 6.1 | 7.1 | 8.2 | 9.2 | 10.2 |
| Parallam ${ }^{\text {PSL }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2.0 E | $31 / 2^{\prime \prime}$ | Moment (ft-lbs) |  |  |  |  | 12,415 | 13,055 | 17,970 | 19,900 | 27,160 | 34,955 | 43,665 |  |
|  |  | Shear (lbs) |  |  |  |  | 6,260 | 6,430 | 7,615 | 8,035 | 9,475 | 10,825 | 12,180 |  |
|  |  | Moment of Inertia (in. ${ }^{4}$ ) |  |  |  |  | 231 | 250 | 415 | 488 | 800 | 1,195 | 1,701 |  |
|  |  | Weight (plf) |  |  |  |  | 10.1 | 10.4 | 12.3 | 13.0 | 15.3 | 17.5 | 19.7 |  |
|  | 51/4" | Moment (ft-liss) |  |  |  |  | 18,625 | 19,585 | 26,955 | 29,855 | 40,740 | 52,430 | 65,495 |  |
|  |  | Shear (lbs) |  |  |  |  | 9,390 | 9,645 | 11,420 | 12,055 | 14,210 | 16,240 | 18,270 |  |
|  |  | Moment of Inertia (in. ${ }^{\text {4 }}$ ) |  |  |  |  | 346 | 375 | 623 | 733 | 1,201 | 1,792 | 2,552 |  |
|  |  | Weight (plf) |  |  |  |  | 15.2 | 15.6 | 18.5 | 19.5 | 23.0 | 26.3 | 29.5 |  |
|  | $7{ }^{\prime \prime}$ | Moment (ft-lbs) |  |  |  |  | 24,830 | 26,115 | 35,940 | 39,805 | 54,325 | 69,905 | 87,325 |  |
|  |  | Shear (lbs) |  |  |  |  | 12,520 | 12,855 | 15,225 | 16,070 | 18,945 | 21,655 | 24,360 |  |
|  |  | Moment of Inertia (in. ${ }^{\text {4 }}$ |  |  |  |  | 462 | 500 | 831 | 977 | 1,601 | 2,389 | 3,402 |  |
|  |  | Weight (plf) |  |  |  |  | 20.2 | 20.8 | 24.6 | 26.0 | 30.6 | 35.0 | 39.4 |  |

## Weyerhaeuser - Trus Joist - LSL - LVL - PSL

## DESIGN PROPERTIES

| ign | $\text { resses }{ }^{(1)}$ | $\begin{aligned} & C_{D}=1.0 \\ & 00 \% \text { Load } \end{aligned}$ | uration) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grade | Orientation | ```G Shear Modulus of Elasticity (psi)``` | $\begin{gathered} \text { Modulus } \\ \text { of Elasticity } \\ (\mathrm{psi}) \end{gathered}$ | $E_{\text {min }}$ Adjusted Modulus of Elasticity (psi) | $F_{b}$ <br> Flexural Stress ${ }^{(3)}$ (psi) | $\begin{gathered} F_{t} \\ \text { Iension } \\ \text { Stress } \\ (\text { psi) } \end{gathered}$ | $\begin{gathered} \mathrm{F}_{c \perp} \\ \text { Compression } \\ \text { Perpendicular } \\ \text { to Grain(5) } \\ (\mathrm{psi}) \end{gathered}$ | Foll $_{\text {al }}$ Compression Parallel to Grain (psi) | $F_{V}$ Horizontal Shear Parallel to Grain (psi) | SG <br> Equivalent Specific Gravity ${ }^{(6)}$ |
| TimberStrand ${ }^{\text {LSL }}$ |  |  |  |  |  |  |  |  |  |  |
| 1.3E | Beam/Column | 81,250 | $1.3 \times 10^{6}$ | 660,750 | 1,700 | 1,075 | 710 | 1,835 | 425 | $0.50{ }^{(7)}$ |
|  | Plank | 81,250 | $1.3 \times 10^{6}$ | 660,750 | $1,900{ }^{(8)}$ | 1,075 | $635{ }^{(9)}$ | 1,835 | 150 | $0.50{ }^{(7)}$ |
| 1.55 E | Beam | 96,875 | $1.55 \times 10^{6}$ | 787,815 | 2,325 | 1,070 ${ }^{(10)}$ | 900 | 2,170 | $310^{(10)}$ | $0.50{ }^{(7)}$ |
| Microllam ${ }^{\text {LVI }}$ |  |  |  |  |  |  |  |  |  |  |
| 2.0 E | Beam | 125,000 | $2.0 \times 10^{6}$ | 1,016,535 | 2,600 | 1,555 | 750 | 2,510 | 285 | 0.50 |
| Parallam ${ }^{\text {e PSL }}$ |  |  |  |  |  |  |  |  |  |  |
| 1.8E | Column | 112,500 | $1.8 \times 10^{6}$ | 914,880 | 2,400(11) | 1,755 | 545 (11) | 2,500 | $190{ }^{(11)}$ | 0.50 |
| 2.0 E | Beam | 125,000 | $2.0 \times 10^{6}$ | 1,016,535 | 2,900 | 2,025 | $625(12)$ | 2,900 ${ }^{(13)}$ | 290 | 0.50 |

(1) Unless otherwise noted, adjustment to the design stresses for duration of load are permitted
in accordance with the applicable code.
(2) Reference modulus of elasticity for beam and column stability calculations, per NDS®.
(3) For $12^{2}$ depth. For other depths, multiply $F_{b}$ by the appropriate factor as follows:

- For IimberStrand ${ }^{\Phi}$ LSL, multiply by $\left[\frac{12}{d}\right]^{0.092}$
- For Microllam ${ }^{\oplus}$ LVL, multiply by $\left[\frac{12}{d}\right]^{0.136} C_{F}$
- For Parallam® PSL, multiply by $\left[\frac{12}{d}\right]^{0.111}$
(4) $F_{1}$ has been adjusted to reflect the volume effects for most standard applications.
(5) $\overline{F_{C L}}$ may not be increased for duration of load.
(6) For lateral connection design only.
(7) Specific gravity of 0.58 may be used for bolts installed perpendicular to face and loaded perpendicular to grain.
(8) Values are for thickness up to $31 / 2$ ".
(9) For members less than $13 /{ }^{\prime \prime}$ thick and in plank orientation, use $\mathrm{F}_{\mathrm{c} 1}$ of 670 psi.
(10) Value accounts for large hole capabilities. See Allowable Holes on page 26.
(11) Value shown is for plank orientation.
(12) Use 750 psi for Parallam® PSL identified with plant number 0579
(13) For column applications, use $\mathrm{F}_{\text {cll }}$ of 500 psi. Alternatively, refer to ESR-1387, Table 1, footnote 15 .

TJ_9000.pdf

General Assumptions for Trus Joist ${ }^{\oplus}$ Beams
" Lateral support is required at bearing and along the span at 24" on-center, maximum.

- Bearing lengths are based on each product's bearing stress for applicable grade and orientation.
- All members $71 / 4^{\prime \prime}$ and less in depth are restricted to a maximum deflection of $5 / 16^{\circ}$.
- Beams that are $134^{\prime \prime} \times 16^{\prime \prime}$ and deeper require multiple plies. Some exceptions allowed when using Weyerhaeuser software.
- No camber.
- Beams and columns must remain straight to within 5 L2/4608 (in.) of true alignment. $L$ is the unrestrained length of the member in feet.
For applications not covered in this brochure, contact your Weyerhaeuser representative.
See pages 28 and 29 for multiple-member beam connections.

TimberStrand $\otimes$ LSL, Microllam@ LVL, and untreated Parallam ${ }^{\otimes}$ PSL are intended for dry-use applications

Plank Orientation


| Span | Condition | 13/4, Width |  |  |  |  |  |  | 31/2" Width (2 ply) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $51 / 22^{\prime \prime}$ | 71/4" | 91/4" | 91/2" | 11/1/4 | 11/8" | $14^{\prime \prime}$ | 51/2" | 71/4" | 91/4" |  | 111/4" | 11/8" |
| $6^{\prime}$ | Total Load <br> Deflection L/240 <br> Min. End/Int. Bearing (in.) | 474 | 954 | 1,285 | 1,329 | 1,656 | 1,781 | 1,961 | 948 | 1,908 | 2,571 | 2,659 | 3,313 | 3,563 |
|  |  | 458 | * | * | * | * | * | * | 916 | * | * | * | * | * |
|  |  | 1.5/3.5 | 2.2/5.5 | 2.9/7.4 | 3.1/7.6 | 3.8/9.5 | 4.1/10.2 | 4.5/11.3 | 1.5/3.5 | 2.2/5.5 | 2.9/7.4 | 3.1/7.6 | 3.8/9.5 | 4.1/10.2 |
| $8^{8}$ | Total Load Deflection L/240 Min. End/lnt. Bearing (in.) | 153 | 342 | 870 | 915 | 1,145 | 1,224 | 1,469 | 307 | 685 | 1,741 | 1,830 | 2,290 | 2,449 |
|  |  | * | * | * | * | * | * | * | * | * | * | * | * | * |
|  |  | 1.5/3.5 | 1.5/3.5 | $2.71 / 6.7$ | 2.817 | 3.5/8.8 | 3.8/9.4 | 4.5/11.3 | 1.5/3.5 | 1.5/3.5 | $2.7 / 6.7$ | 2.8/7 | 3.5/8.8 | 3.8/9.4 |
| $9^{9}-66^{\prime \prime}$ | Total LoadDeflection $\mathbf{L / 2 4 0}$Min. End/lnt. Bearing (in.) | 77 | 174 | 615 | 647 | 888 | 982 | 1,212 | 154 | 349 | 1,231 | 1,294 | 1,776 | 1,965 |
|  |  | * | * | 543 | 585 | * | * | * | * | * | 1,086 | 1,171 | * | * |
|  |  | 1.5/3.5 | 1.5/3.5 | 2.2/5.6 | 2.4/5.9 | 3.2/8.1 | 3.6/8.9 | 4.4/11 | 1.5/3.5 | 1.5/3.5 | 2.215.6 | 2.4/5.9 | 3.2/8.1 | 3.6/8.9 |
| $10^{\prime}$ | Total Load <br> Deflection $\mathrm{L} / 240$ <br> Min. End $/$ Int. Bearing (in.) | 62 | 142 | 555 | 583 | 801 | 886 | 1,137 | 124 | 284 | 1,110 | 1,167 | 1,602 | 1,772 |
|  |  | * | * | 470 | 506 | * | * | * | * | * | 940 | 1.013 | * | * |
|  |  | 1.5/3.5 | 1.5/3.5 | 2.1/5.3 | 2.215 .6 | 3.1/7.7 | 3.4/8.5 | 4.4/10.9 | 1.5/3.5 | 1.5/3.5 | 2.1/5.3 | 2.215 .6 | 3.1/7.7 | 3.4/8.5 |
| 12' | Total Load <br> Deflection $\mathrm{L} / 240$ <br> Min. End/Int. Bearing (in.) |  | 67 | 367 | 397 | 554 | 613 | 835 | 57 | 135 | 735 | 794 | 1,109 | 1,227 |
|  |  |  |  | 279 | 301 | 488 | 568 | * | * | * | 558 | 602 | 976 | 1,137 |
|  |  |  | 1.5/3.5 | 1.774.3 | 1.8/4.6 | 2.6/6.4 | 2.817 .1 | 3.9/9.6 | 1.5/3.5 | 1.5/3.5 | 1.774.3 | 1.8/4.6 | 2.6/6.4 | 2.877.1 |
| 14' | Total Load Deflection L/240 Min. End/Int. Bearing (in.) |  |  | 233 | 252 | 405 | 449 | 611 |  | 70 | 466 | 505 | 811 | 898 |
|  |  |  |  | 178 | 193 | 314 | 367 | 585 |  | * | 357 | 386 | 629 | 734 |
|  |  |  |  | 1.5/3.5 | 1.5/3.5 | 2.2/5.5 | 2.4/6.1 | 3.3/8.3 |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 2.2/5.5 | 2.4/6.1 |
| 16'-6" | Total Load Deflection L/240 Min. End/Int. Bearing (in.) |  |  | 142 | 154 | 255 | 299 | 438 |  |  | 285 | 308 | 510 | 598 |
|  |  |  |  | 110 | 119 | 195 | 228 | 367 |  |  | 220 | 238 | 391 | 457 |
|  |  |  |  | 1.5/3.5 | 1.5/3.5 | 1.6/4.1 | 1.9/4.8 | $2.8 / 7$ |  |  | 1.5/3.5 | 1.5/3.5 | 1.6/4.1 | 1.9/4.8 |
| 18'-6" | Total Load Deflection L/240 Min. End/Int. Bearing (in.) |  |  | 100 | 108 | 181 | 212 | 345 |  |  | 200 | 217 | 362 | 425 |
|  |  |  |  | 78 | 85 | 140 | 164 | 264 |  |  | 157 | 170 | 280 | 328 |
|  |  |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.9 | 2.5/6.2 |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.9 |
| 20' | Total Load <br> Deflection $\mathrm{L} / 240$ <br> Min. End/lnt. Bearing (in.) |  |  | 78 | 85 | 143 | 168 | 274 |  |  | 157 | 171 | 286 | 336 |
|  |  |  |  | 62 | 67 | 111 | 130 | 211 |  |  | 125 | 135 | 223 | 261 |
|  |  |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 2.1/5.4 |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 |
| 22' | Total Load <br> Deflection L/240 <br> Min. End/Int. Bearing (in.) |  |  | 58 | 63 | 106 | 125 | 206 |  |  | 116 | 126 | 213 | 251 |
|  |  |  |  | 47 | 51 | 84 | 98 | 160 |  |  | 94 | 102 | 168 | 197 |
|  |  |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.8/4.5 |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 |
| 24' | Total Load <br> Deflection $\mathrm{L} / 240$ <br> Min. End/lnt. Bearing (in.) |  |  |  |  | 81 | 95 | 158 |  |  | 87 | 95 | 162 | 191 |
|  |  |  |  |  |  | 65 | 76 | 124 |  |  | 73 | 79 | 130 | 153 |
|  |  |  |  |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.8 |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 |
| 26' | Total Load <br> Deflection L/240 <br> Min. End/Int. Bearing (in.) |  |  |  |  | 62 | 74 | 123 |  |  | 67 | 73 | 125 | 148 |
|  |  |  |  |  |  | 51 | 60 | 98 |  |  | $3 /$ | 62 | 102 | 120 |
|  |  |  |  |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 |
| $28^{\prime}$ | Total Load <br> Deflection L/240 <br> Min. End/Int. Bearing (in.) |  |  |  |  |  | 58 | 98 |  |  | 52 | 56 | 98 | 117 |
|  |  |  |  |  |  |  | 48 | 78 |  |  | 46 | 50 | 82 | 97 |
|  |  |  |  |  |  |  | 1.5/3.5 | 1.5/3.5 |  |  | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 | 1.5/3.5 |
| $30^{\prime}$ | Total Load <br> Deflection L/240 <br> Min. End/Int. Bearing (in.) |  |  |  |  |  |  | 78 |  |  |  |  | 78 | 93 |
|  |  |  |  |  |  |  |  | 64 |  |  |  |  | 67 | 79 |
|  |  |  |  |  |  |  |  | 1.5/3.5 |  |  |  |  | 1.5/3.5 | 1.5/3.5 |

TJ_9000.pdf

## Selection

1. Calculate total beam load
2. Choose beam span in chart
3. Find section to carry load
or
Propping
4. Calculate shear and moment
5. Use properties chart to find section
6. Include adjustment factors: $\mathrm{C}_{\mathrm{D}}, \mathrm{C}_{\mathrm{V}}$


LVI
Example - Beam 4
Given: $\quad$ span $=24 \mathrm{ft}$.
D 6 psf Lr 20 psf


1. Calculate total beam load
2. Choose beam span in chart

LoAD in Ply
3. Find section to carry load

$$
D+L_{r}=6+20=26 \text { PSF }
$$

$$
26\left(5^{\prime}\right)=130 \text { PLF }
$$

Example
Beam 4

Span = 24 ft
Load $=130$ plf Lr = 100 plf

Pick $13 / 4$ " x 14 "



## LVI - PS - ISL

Example - Beam 4

Given: $\quad$ span $=24 \mathrm{ft}$. D 6 psf Lr 20 psf 130 pf

1. Calculate total beam load
2. Calculate shear and moment
3. Use properties chart to find section
4. Check stresses
5. Check deflection


$V_{\text {max }}=\frac{\omega l}{2}=\frac{130(24)}{2}=1560 *$

Weyerhaeuser - Crus Joist - LSL - LVL - PSL
DESIGN PROPERTIES


LV
Example - Beam 4

Given: $\quad$ span $=24 \mathrm{ft}$.
D 6 psf Lr 20 psf
130 vlf (total load)
M = 9360 ft -lbs
$\mathrm{V}=1560 \mathrm{lbs}$
3. Use properties chart to find section

$$
\begin{aligned}
& H_{\text {MAX }}=\frac{w l^{2}}{8}=\frac{130(24)^{2}}{8}=9360^{1 . *} \\
& V_{\text {max }}=\frac{\omega l}{2}=\frac{130(24)}{2}=1560^{*}
\end{aligned}
$$

$$
\begin{aligned}
& \text { TRY LVL } 2.0 E \frac{13 / 4^{\prime \prime} \times 111 / 4 "}{\prime \prime} \\
& S_{x}=\frac{b d^{2}}{6}=\frac{1.75^{\prime \prime}(11.25)^{2}}{6}=36.91 \mathrm{~m}^{3} \\
& \underline{f_{b}}=\frac{M}{S_{x}}=\frac{9360(12)}{36.91}=3042 \mathrm{ps} \\
& A=1.75(11.25)=19.68 \mathrm{~m}^{2} \\
& f_{V}=\frac{3}{2} \frac{V}{A}=1.5 \frac{1560^{444}}{19.68}=118.8 \mathrm{ps}
\end{aligned}
$$

## Weyerhaeuser - Crus Joist - LSL - LVL - PSL

DESIGN PROPERTIES

Design Stresses ${ }^{(1)}$ (100\% Load Duration)

(1) Unless otherwise noted, adjustment to the design stresses for duration of load are permitted in accordance with the applicable code.
(2) Reference modulus of elasticity for beam and column stability calculations, per NOSe
(3) For $12^{" 1}$ depth. For other depths, multiply $F_{b}$ by the appropriate factor as follows:

- For TimberStrand ${ }^{\oplus}$ LSL, multiply by $\left[\frac{12}{4}\right]_{4}^{0.092}$
$\longrightarrow-$ For Microllam ${ }^{\oplus}$ LVL, multiply by $\left[\frac{12}{d}\right]^{0.136}$ CF
- For Parallam@ PSL, multiply by $\left[\frac{12}{d}\right]$
(4) $F_{t}$ has been adjusted to reflect the volume effects for most standard applications.
(5) $F_{c \perp}$ may not be increased for duration of load.
(6) For lateral connection design only.
(7) Specific gravity of 0.58 may be used for bolts installed perpendicular to face and loaded perpendicular to grain.
(8) Values are for thickness up to $31 / 2^{\prime \prime}$.
(9) For members less than $134^{\prime \prime}$ thick and in plank orientation, use $F_{c \perp}$ of 670 psi.

10) Value accounts for large hole capabilities. See Allowable Holes on page 26.
(11) Value shown is for plank orientation.
(12) Use 750 psi for Parallam® PSL identified with plant number 0579
(13) For column applications, use $\mathrm{F}_{\text {cl }}$ of 500 psi. Alternatively, refer to ESR -1387, Table 1, footnote 15 .


University of Michigan, TCAUP

LVI
Example - Beam 4
Given: $\quad$ span $=24 \mathrm{ft}$.
D 6 psf Lr 20 psf 130 pf

Try:
$13 / 4^{\prime \prime} \times 11.25^{\prime \prime}$
4. Check stresses

$$
13 / 4 " \times 11.25 "
$$

## $F_{b}$ Adjustment

$$
\begin{aligned}
& C_{D}=1.25^{r} \\
& C_{V}=\left[\frac{12}{d}\right]^{0.136}=\left(\frac{12}{14}\right)^{0.136}=0.979 \\
& C_{L}(\text { PER NDS 3.3.3) } \\
& \frac{\text { BRACED BY RAFTERS }}{} \therefore C_{L}=1.0 \\
& C_{M}, C_{t}, C_{r}=1.0-
\end{aligned}
$$

$$
\begin{aligned}
& L_{V L} 2.0 E \quad 13 / 4^{\prime \prime} \times 11^{\prime} / 4^{\prime \prime} \\
& F_{b}=2600 \mathrm{ps1} \\
& F_{V}=285 \mathrm{ps1} C_{D} \quad C_{F} \\
& F_{b}^{\prime}=2600(1.25)(0.979)=3182 \mathrm{psi} \\
& F_{b}^{\prime}=3182>3042=f_{b} \text { ok V } \\
& F_{V}^{\prime}=285(1.25)=356 \mathrm{psi} \\
& F_{V}^{\prime}=356>118=F_{V} \text { ok }
\end{aligned}
$$

Given: $\quad$ span $=24 \mathrm{ft}$.
Lr 20 psf 100 pf
5. Check deflection
for Lr < L/240
IBC Table 1604.3 DEFLECTION LIMITS $\mathrm{a}, \mathrm{b}, \mathrm{c}, \mathrm{n}, \mathrm{i}$

| CONSTRUCTION | $L$ or $/ L_{r}$ | S or $W^{\mathbf{t}}$ | $D+L^{\mathrm{d}, \mathbf{g}}$ |
| :--- | :---: | :---: | :---: |
| Roof members: |  |  |  |
| Supporting plaster or stucco ceiling | $/ / 360$ | $/ / 360$ | $/ / 240$ |
| Supporting nonplaster ceiling | $/ / 240$ | $/ / 240$ | $/ / 180$ |
| Not supporting ceiling | $/ / 180$ | $/ / 180$ | $/ / 120$ |
| Floor members | $/ / 360$ | - | $/ / 240$ |
| Exterior walls: |  |  |  |
| With plaster or stucco finishes | - | $/ / 360$ | - |
| With other brittle finishes | - | $/ / 240$ | - |
| With flexible finishes | - | $/ / 120$ | - |
| Interior partitions: |  |  |  |
| With plaster or stucco finishes | $/ / 360$ | - | - |
| With other brittle finishes | $/ / 240$ | - | - |
| With flexible finishes | $/ / 120$ | - | - |
| Farm buildings | - | - | $/ / 180$ |
| Greenhouses | - | - | $/ / 120$ |

$1.75^{\prime \prime} \times 11.25^{\prime \prime}$
$I=\frac{b d^{3}}{12}=20 \mathrm{am}^{4}$
$\begin{aligned} \Delta & =\frac{5 w 8^{4}}{384 E 1}=\frac{5(100)(24)^{4}(1728)}{384\left(2.0 \times 10^{6}\right) \frac{2088}{[244]}} \\ & =\frac{1.8^{\prime \prime}\left[1.5^{\prime}\right]}{\frac{L}{240}}=\frac{24(12)}{240}=1.2^{\prime \prime}<1.8^{\prime \prime} \quad \therefore \text { FALLS }\end{aligned}$
$1.75^{\prime \prime} \times 14^{\prime \prime}$
$I=\frac{6 d^{3}}{12}=\frac{1.75(14)^{3}}{12}=400 \mathrm{~m}^{4}$
$\Delta=\frac{5 w l^{4}}{384 E I}=\frac{5(100)(24)^{4}(1728)}{384(2000000)(400)}=0.93 \mathrm{~m}$
$\frac{h}{240}=\frac{24(12)}{240}=1.20>0.93 \mathrm{~m}$ ok

Wood
Slide 27 of 27

## Weyerhaeuser - Crus Joist - LSL - LVL - PSL DESIGN PROPERTIES



